

# Analysis of on Load Tap Changing Transformer for Substation

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These systems usually possess 33 taps (one at the centre "Rated tap and sixteen to increase and decrease the turn ratio) and allow for  $\pm 8\%$  variation (each step providing 1.65% variation) from the nominal transformer rating which, in turn, allow for stepped voltage regulation of the output.

Tap changers are often placed on the high voltage (low current) transformer winding for easy access and to minimize the current load during operation. ON-Load Tap Change: Most of the Generating Station, Substation system having Power Transformer with On-Load Tap Changer (OLTC). Not only in Generating Station Transformer but also in Distribution Class Transformer too. In this substation, there are three windings; such as primary winding, secondary winding and tertiary winding. Among them, we will neglect the tertiary winding which is used for residential houses.

## 2. LITERATURE REVIEW

Transformers are essential for the transmission, distribution, and utilization of alternating current electrical energy. In more technical terms, a power transformer is composed of two or more windings which, by electromagnetic induction, transform a system of alternating voltage and current into another system of voltage and current for the purpose of transmitting electrical power. Mainly the regulation of voltage is achieved by altering the ratio of transformation by tapping the winding, so as to alter the number of turns. The process of altering the ratio of transformation by tapping the windings is termed as tap changing. Tapping may be changed mainly in two different ways; When the transformer is disconnected from the supply, called as, offload tap changing. When the transformer is operating on load (without de-

## ABSTRACT

On-load tap changing transformers play important roles in any modern power system since they allow voltages to be maintained at desired levels despite load changes. Traditionally, on-load tap changer is a complex mechanical device, which has some deficiencies. On-load tap changer of a transformer is presented, which can eliminate excessive conduction losses and suppress the arcing in the diverter switch, which is inherent in traditional on-load transformer tap changers. The OLTC provides uninterrupted voltage regulation of transformers under load. The transformer is equipped with a tapped winding whose tapping's are connected with the tap selector of the OLTC. Most of the current commercially available automatic voltage regulators, just measure the low voltage side of the power transformer in order to control OLTC position. In this to improve tap-changer control in order to perform properly also during a stressed situation in the 230/33 kV regulating power transformer for the substation.

**KEYWORDS:** load changes, tap changer, diverter switch, voltage regulation, power transformer for substation

## 1. INTRODUCTION

A tap changer is a mechanism in transformers which allows for variable turn ratios to be selected in discrete steps. Transformers with this mechanism obtain this variable turn ratio by connecting to a number of access points known as taps along either the primary or secondary winding.

energized), known as on-load tap changing. During offload tap changing, the transformer is completely de-energized, in order to avoid arcing at the point of breath.

The method of offload tap changing is not suitable for large power supply systems. This system call for power transformer with a voltage regulating winding, the tapping of which are changed over under loaded condition by on-load tap changer. The schemes employed for on-load tap changer involved the use of more complicated and expensive tap changing equipment. As such, power transformers with on-load tap changing arrangement are larger in size, have a greater height and consequently more costly compared to the transformer of same output and voltage, but provided with off-load tap changer. Due to the higher cost of the on-load tap changer, normally small and medium rating of transformers is provided with off-load tap changer. Larger rating transformers are provided with on-load tap changer because frequent discontinuity of power cannot be tolerated by the power system network.

## 3. STUDYING DESIGN THEORY OF OLTC TRANSFORMER

For design and calculation of on-load tap changing transformer are calculated by using the following equations.

e.m.f per turns,

$$E_t = 4.44 f B_m A_t \quad (1)$$

$$E_t = K \sqrt{\frac{kVA}{\text{phase}}} \quad (2)$$

**Table1. Values of Factor, K**

Type of Transformer	Factor, K
Three phase core type (power)	0.6 to 0.7
Three phase core type (distribution)	0.45 to 0.5
Three phase shell type	1.2 to 1.3
Single phase core type	0.75 to 0.8
Single phase shell type	1 to 1.1

$$A_i = k_s A_{gi} \quad (3)$$

$k_s$  = stacking factor, usual value is 0.85 – 0.9

Output equation of three phase transformer  
 $Q = 3.33 f B_m \delta k_i A_w A_i \times 10^{-3} \text{ (kVA)} \quad (4)$

$$\eta = \frac{\text{Output power}}{\text{Output power} + \text{Total losses}} \times 100 \% \quad (5)$$

Number of turns per phase,

$$T_1 = T_2 \times \frac{V_1}{V_2} \quad (6)$$

### 3.1 Specific Magnetic loading, $B_m$

Normally two types of sheet steel are used for the core and yoke of transformers

A. hot rolled silicon steel.

B. cold rolled grain oriented silicon steel.

Using hot rolled silicon steel.

Power transformers -1.2 to 1.4 Tesla

Distribution transformers - 1.1 to 1.3 Tesla

Using hot rolled silicon steel.

Power transformers -1.5 to 1.7 Tesla

Distribution transformers -1.4 to 1.5 Tesla

Window space factor  $K_w = \frac{10}{30 + kV1}$

**Table 2.Window Space Factor  $k_w$** 

kVA	3.3kV	11kV	33kV	110kV
100	0.27	0.2	0.14	-
1000	0.38	0.28	0.2	0.15
2000	0.4	0.3	0.24	0.16
5000	0.42	0.34	0.26	0.18
10000	0.45	0.37	0.29	0.2

Effects of kVA rating on the above value of window space are the following facts.

1. The above values are quite satisfactory for transformers between 50 to 250 kVA.
2. The above values may be reduced by 5 to 20% for transformers rated between 5kVA to 50kVA.
3. The above value may be increased by 5 to 20% for transformer above 250 kVA.

The net cross-sectional area of the core

### 3.2 Current Density, $\delta$

The current density for H.V winding should be taken comparatively higher, compared to the current density for L.V winding, because cooling conditions are better in the L.V winding.

Distribution transformers -2.00 to 2.5 A/mm<sup>2</sup>  
 Power transformers - 2.3 to 3.5 A/mm<sup>2</sup>  
 Large transformers with forced -3 to 4.5 A/mm<sup>2</sup>

Area of the window

$$A_w = L(D-d)$$

Width of the window

$$b_w = (D-d) \text{ for various stepped core}$$

The overall length of the yoke,

$$W = 2D + 0.9d \text{ (for three-phase, three stepped)}$$

Area of yoke

$$A_y = 1.1 \text{ to } 1.15 A_i$$

Width of the yoke

$$b_y = 0.9 d \text{ (for three stepped core)}$$

## 4. SPECIFICATIONS TO DESIGN

A design based on the following typical specifications.

Rating -100MVA

No. of phase -Three phase

Frequency -50Hz

Voltage ratio -230/33kV at no-load

Percentage tapping - $\pm 8 \times 1.65\%$

No. of tapping -17 positions

Connection -HV star, LV star

Cooling -Oil natural air natural (ONAN)

Type -Core type, cold-rolled silicon steel sheet

Location -Outdoor

## 5. RESULT DATA OF ON LOAD TAP CHANGING TRANSFORMER

**Total iron losses = 0.2 % (within limit)**

The iron losses in small transformer may be of the order of 0.5 to 1 % of rated output. In large and small transformers, iron losses should be within 0.2 to 0.5 % of rated output.

**Percentage no-load current = 0.53% (within limit)**

The no-load current of a small transformer may be of the order of 3 to 5 percent of the rated current, whereas in medium transformers, it varies from 1 to 3 percent. In the case of large transformers, no-load current may be from 0.5 to 2 percent of the rated current within the proper range.

### Tapping result

Rated tap and sixteen to increase and decrease the turn ratio and allow for Rated tap and sixteen to increase and decrease the turn ratio and allow for  $\pm 8\%$  variation (each step proving 1.65% variation) from the nominal transformer rating which, in turn, along for stepped voltage regulation of the output.

### Efficiency

At full load (0.8 p.f) = 99% (within limit)

At full load (unity) = 99% (within limit)

At half load (0.8 p.f) = 98.8% (within limit)

At  $\frac{3}{4}$  load (0.8 p.f) = 99.2% (within limit)

The efficiency of the small transformer may be of the order of 98%, whereas for medium and large transformer, its values are from 98.0 to 99.2%

**Table3. OLTC Positions for 230kV Side of 100MVA Power Transformer**

Tap Position	Tap	Number of turns(turns)	H.V Side Voltage(Volts)
1	1.65%	2408	260360
2	3.30%	2363	256565
3	4.95%	2320	252770
4	6.60%	2280	248975
5	8.25%	2238	245180
6	9.90%	2200	241385
7	11.55%	2162	237590
8	13.20%	2126	233765
9	0%	2090	230000
10	-1.65%	2057	226205
11	-3.30%	2024	222410
12	-4.95%	1992	218615
13	-6.60%	1961	214820
14	-8.25%	1931	211025
15	-9.90%	1902	207230
16	-11.55%	1874	203435
17	-13.2%	1847	199640

## 6. CONCLUSIONS

This thesis was intended for design calculation of OLTC power transformer. OLTC theory, operation and example application with Myaukpyin Substation is also described in this thesis. Presently available technical solutions enable the production of OLTCs that are reliable and meet the same life expectancy as transformers. At the present time and for the foreseeable future, the proper implementation of the vacuum switching technology in OLTCs provides the best formula of quality, reliability, and economy achievable a maintenance-free design.

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